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X-ray Tomographic Micro-Particle Velocimetry in Porous Media

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Fluid flow through intricate confining geometries often exhibits complex behaviors, certainly in porous materials, e.g. in groundwater flows or the operation of filtration devices and porous catalysts. However, it has remained extremely challenging to measure 3D flow fields in such micrometer-scale geometries. Here, we introduce a new 3D velocimetry approach for optically opaque porous materials, based on time-resolved X-ray micro-computed tomography (CT). We imaged the movement of X-ray tracing micro-particles in creeping flows through the pores of a sandpack and a porous filter, using laboratory-based CT at frame rates of tens of seconds and voxel sizes of 12 m. For both experiments, fully three-dimensional velocity fields were determined based on thousands of individual particle trajectories, showing a good match to computational fluid dynamics simulations. Error analysis was performed by investigating a realistic simulation of the experiments. The method has the potential to measure complex, unsteady 3D flows in porous media and other intricate microscopic geometries. This could cause a breakthrough in the study of fluid dynamics in a range of scientific and industrial application fields.



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energy or carbon storage reservoirs (Mouli-Castillo et al., 2019; Bui et al., 2018), and 4 the performance of filtration devices, fuel cells and catalysts (Miele, Anna, and Dentz, 5 2019; Mularczyk et al., 2020). The intricate pore geometries in such materials can lead to 6 complex phenomena, particularly during solute and colloid transport (Zhang et al., 2021; 7 Iaffner and Mirbod, 2020; Russell and Bedrikovetsky, 2021), multiphase flows (Blunt, 2017; Singh et al., 2019) and non-Newtonian flows (An et al., 2022). While experiments n simplified (often 2D) model geometries give valuable insights on flow behavior in the 10 onfinement of generic pore walls (Primkulov et al., 2019; Lenormand, Zarcone, and Sarr, 11 983; Holtzman, 2016; Datta, Dupin, and Weitz, 2014), the physical interactions in the 12 omplex 3D pore networks encountered in many applications remain difficult to probe. This 13 important as highly irregular pore geometry and connectivity are known to influence the 14 merging behavior at the macro-scale in a non-trivial way, due to the non-linearity of many 15 ow processes in porous media (Mascini et al., 2021; Ling et al., 2017; McClure, Berg, and 16 rmstrong, 2021). Recent pore-scale numerical simulation methods can - to a certain extent 17 be applied to study these porous media, but often still come with significant uncertainties 18 the incorporated physical assumptions and materials properties (Zhao et al., 2019; Ye 19 al., 2019). Furthermore, such methods are in many cases severely restricted by either the 20 computational time, domain size or accuracy. There is thus an important need for *in-situ* 21 experimental measurements to study 3D porous media flows at the scale of the flow-confining 22 pore geometries (nm to mm). 23 For the wider field of experimental fluid mechanics, the introduction of methods to mea-24 sure 3D flow and pressure fields has been a turning point, as reviewed by Discetti and 25

Fluid dynamics in porous materials play an important role in nature and in industry, e.g. groundwater flow in aquifers (Mercer and Cohen, 1990), gas-brine flow in geological

INTRODUCTION

1 I.

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Coletti (2018). However, this has not been applicable to a majority of porous materials of 26 interest to the research community, due to the optical opacity of these materials. Most flow 27 field measurements are based on optical particle velocimetry, using visible light to image 28 the movement of flow-tracing particles in (index-matched) fluids over time. With micro-29 particles and microscopes, this principle can be used to measure micron-scale flow fields in 30 transparent 2D micromodels (Roman et al., 2015; Zarikos et al., 2018) and even in op-31



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tically transparent 3D porous media, using multi-camera set-ups (Schanz, Gesemann, and 32 Schröder, 2016), astigmatic optics (Franchini et al., 2019) or confocal microscopy (Datta 33 al., 2013; Datta, Ramakrishnan, and Weitz, 2014). However, these techniques are in-34 herently unsuited for optically opaque - and thus most - porous materials. An alternative 35 method is to measure fluid propagators using (pulsed-field gradient) magnetic resonance 36 imaging (Gladden and Sederman, 2013). While having several advantages, including not 37 quiring tracers, this method has only recently started to reach the required micron-scale 38 spatial resolutions (de Kort et al., 2019). Several hours are required to measure a single flow 39 field at this resolution, restricting its applicability to static flow fields. 40

In this paper, we introduce a 3D micro-particle velocimetry method for porous media by 41 leveraging the penetrating power of X-rays. Contrary to previous methods, the approach is 42 applicable to tortuous, spatially varying 3D flow fields common in porous media, and can be 43 xtended to unsteady flows. Prior approaches to X-ray based particle velocimetry started 44 with 2D, radiography-based measurements, which did not yield 3D information (Lee and 45 Kim, 2003). This was followed by methods that reconstructed 3D flow fields from correlations within radiography sequences, taken from different viewing angles (Fouras et al., 2007; 47 Dubsky et al., 2012; Baker et al., 2018). While high particle velocities could be measured 48 because radiographs can be acquired mere milliseconds apart, these methods have only been 49 pplied to fairly homogeneous flows in e.g. a blood vessel, and it is unclear how well suited 50 their reconstruction algorithms are to complex flow fields in porous media. The alternative 51 method we adopt here is X-ray micro-computed tomography (CT), an inherently 3D, non-52 destructive and micrometer-scale technique (Cnudde and Boone, 2013; Wildenschild and 53 Sheppard, 2013), to reconstruct a time series of 3D images of flow-tracing particles. The 54 challenge is to precisely resolve the locations of the tracer particles at a sufficiently high 55 ame rate. For their motion to be representative of the flow, these particles should be small 56 and close in mass density to the liquid to negate inertial and gravitational effects. However, 57 this tends to negatively affect the particles' visibility in X-ray imaging. Furthermore, CT 58 imaging typically takes tens of minutes to acquire a 3D image, which is too slow to track 59 the particle movement. Time resolutions on the scale of (tens of) seconds have only be-60 ome possible at synchrotrons a few years ago (Berg *et al.*, 2013), and even more recently 61 laboratory-based CT scanners (Bultreys et al., 2016). in 62

⁶³ Very recently, Mäkiharju et al. (2022) provided a proof-of-concept that flow tracer parti-

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cles (60 m large silver-coated hollow glass spheres) in a cylindrical tube could be visualized 64 with laboratory-based CT at frame rates on the order of seconds. Here, we present the 65 first successful CT-based particle velocimetry measurements of creeping single-phase flow 66 in porous media, namely a sandpack and a sintered glass filter. Our method yields fully 67 3D, 3-component velocity fields, by tracing the movement of thousands of individual silver-68 coated micro-spheres with a mean diameter of approximately 20 m. The measurements were 69 erformed using a laboratory-based CT scanner at a voxel size of 12 m and an acquisition 70 time of 70s per scan, with a total measurement time of 30 to 45 minutes. 71

In the following, we first introduce the basic concepts of particle tracking velocimetry 72 in Section IIA. The experimental workflow is described in Section IIB. We used a La-73 grangian Particle Tracking approach to identify individual particle trajectories in the image, 74 and interpolated the resulting velocity data points to find velocity fields, as explained in 75 Section II C. The method was validated on a realistic numerical simulation of an imaging 76 experiment, which provided ground-truth data to validate particle locations and velocities. 77 The generation of this dataset is treated in Section IID. The results of the experiments and 78 the validation are discussed in Section III. 79

80 II. MATERIALS AND METHODS

81 A. Introduction to particle tracking velocimetry

Particle velocimetry (PV) methods work by computing the displacement of flow tracer particles in a time series of images. Before introducing specific approaches, it is useful to discuss following general considerations when selecting or applying these methods:

• The *sampling density* of the resulting velocity field is the density of the cloud of points in which particles were detected and velocities could thus be measured. This has the potential to improve with longer measurement time or denser particle seeding, as well as with the resolution of the particle images.

• The *measurement time* refers to the time needed to acquire all the data to reconstruct a velocity field. This determines whether changes in (unsteady) flows over time can be measured.



• The *frame interval* is the time interval between consecutive particle images (frames). To track the paths of fast-moving particles, this time interval needs to be small enough.

• The *acquisition time* is the time to acquire a single frame. This needs to be small enough to accurately measure the particle positions, as their motion would otherwise cause blurring and other image artifacts. In optical imaging, the frame interval is larger than or equal to the acquisition time, but in our method this is not necessarily the case, as discussed in Section II B.

• The *particle seeding concentration* is the amount of particles in a unit volume of liquid. Higher concentrations can improve the spatial or temporal resolution, but come at the cost of higher computational complexity. In porous media, high seeding concentrations may also induce pore clogging.

• The *tracer fidelity* refers to the need for good flow tracers to follow the flow lines of the liquid, rather than be significantly influenced by inertia or gravity. Particles should thus have a small Stokes number and a small ratio of gravitational settling velocity to flow velocity (Melling, 1997). This depends on the liquid's viscosity and on the size and material density of the particles.

There are two main classes of approaches to PV. The first and most well-known, particle 108 image velocimetry (PIV), yields a flow field from as little as two snapshots of the particles, 109 by dividing the images into small windows that typically contain multiple particles, and 110 investigating correlations between these windows in consecutive time steps (Raffael et al., 111 2018). Particle tracking velocimetry (PTV, also called Lagrangian Particle Tracking), on the 112 other hand, identifies the locations of individual particles as they travel throughout many 113 images. PIV tends to have a better temporal resolution because it requires fewer particle 114 images and deals better with high seeding concentrations, while PTV yields more precisely 115 localized velocity information, as well as Lagrangian properties of the flow (Ouellette, Xu, 116 and Bodenschatz, 2006). 117

In this work, we employ PTV, for two main reasons. First, we aim to measure flows in geometries bound by irregular pore walls, which means that the spatial discretization of PIV into interrogation windows may cause issues. Second, out of concern to avoid significant pore clogging by particle straining (Molnar *et al.*, 2015), we have kept the seeding concentrations

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1.

Experiments

Flow experiments

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gium), sieved to retain the fraction of grains between 500 and 710 m. The grains were poured into a viton sleeve of 4 mm diameter mounted in a flow cell, to a sample height of approximately 20 mm. The second was a cylindrical sintered glass filter of 4 mm diameter and 10 mm height, with nominal pore sizes between 160 and 250 m (ROBU P0, Germany), in a viton sleeve. Image-based estimates of the porosity and mean pore (throat) sizes of the samples are listed in Table I. Both samples were mounted into a vertically-oriented, X-ray

In the following, we first describe how the flow experiments were performed and then pro-

We present velocimetry experiments on two porous samples: a sand pack and a porous

glass filter. The first sample was a construction-grade sand used in mortars (HUBO, Bel-

vide a detailed description of the tracer particle suspension used in these experiments, which

consisted of silver-coated hollow glass spheres in a highly viscous glycerol-water mixture.

relatively low - making PTV the more favorable option.

ransparent Hassler-type flow cell (RS Systems, Norway). We avoided flow from bypassing 136 the sample by pressurizing the sleeve around the samples with a confining pressure of 2 137 MPa. The liquids were injected from the bottom to the top of the samples. The flow cell 138 was mounted on the Environmental CT scanner (EMCT) at Ghent University's Centre for 139 X-ray Tomography: a fast-scanning system which does not rotate the sample like most CT 140 scanners, but instead rotates a source-detector system on a gantry around it. A detailed 141 description of the scanner and its application to fast imaging can be found in Dierick et al. 142 (2014) and Bultreys et al. (2016). A schematic of the setup is shown in Figure 1. 143

Before the velocimetry experiment, the samples were saturated with the unseeded glycerol-water liquid by flooding more than 50 pore volumes of liquid through the sample at a high flow rate, namely a Darcy velocity (fluid flux) of 2 mm/s, to mobilize trapped air. Then, a high-quality CT scan at 6 m voxel size was made of the field-of-view of the experiment: a section of the sample near the inlet, approximately 6.3 mm high and containing its full diameter (2200 projections, 110 kV accelerating voltage, 8W X-ray power, 550 ms

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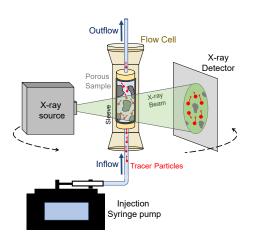


FIG. 1: A schematic of the experimental setup used in this work (not drawn to scale). The samples were 4 mm in diameter and 10 to 20 mm high.

¹⁵⁰ integrated exposure time per projection).

To start the experiment, the tracer particle suspension was drawn up in high-precision 151 glass syringes (Hamilton GasTight Syringe models 1001 and 1002, USA) and injected into the 152 sample at the flow rates listed in Table I, using a Harvard PHD Ultra syringe pump (Harvard, 153 USA). The tracers were injected from the bottom-side of the sample, via PTFE tubing. The 154 imposed constant volumetric flow rates in the experiments were set to arrive at an estimated 155 average interstitial velocity around 1 voxel per scanner rotation (0.5 voxels/frame due to the)156 interleaved reconstruction procedure explained below). These rates were at least 10 times 157 larger than the minimum setting of the syringe pump, ensuring smooth flow. The pump 158 accuracy and reproducibility were respectively 0.25% and 0.05%. After assessing that the 159 tracer particles were present in the sample by radiography, continuous CT acquisitions of 160 either 30 or 40 back-to-back rotations were started, at 70s per full rotation and 11.8 m voxel 161 size (700 projections/rotation, 100 ms exposure time, 60 kV accelerating voltage, 8W X-ray 162 power). 163

After the experiment, the data were reconstructed into time series of 3D frames using a filtered back projection algorithm (Tescan XRE, Belgium), taking 700 projections per frame and 350 projections in between each two frames. This resulted in an "interleaved" time

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¹⁶⁷ series with a frame interval of 35 s and an acquisition time of 70 s. An intuitive way to ¹⁶⁸ understand the resulting data is to compare it to an interleaved stream of images from two ¹⁶⁹ cameras with staggered trigger time, so that the exposures of each two consecutive frames ¹⁷⁰ overlap by 50%. This reduced the maximum distance traveled by a particle between two ¹⁷¹ consecutive frames, which was beneficial for the particle tracking algorithm.

Minor amounts of particle retention were found during visual inspection of cross-sectional 172 slices of the reconstructed images (e.g. Figure 12 in the Appendix), and were deemed to 173 have a limited effect on the velocimetry results as pore clogging was negligible. However, 174 this issue did cause several failed experimental trials during the method's development. 175 Its effects typically became severe after pumping a few pore volumes (i.e. tens of L) of 176 he tracer-seeded liquid through the imaged part of the sample. During both experiments, 177 which took respectively 46 and 35 minutes for the sandpack and the porous glass filter, 178 only 1.5 L of liquid (approximately 5% of the imaged pore volume) was pumped. Carefully 179 timing the arrival of the tracers with the start of the acquisition was thus key. This was 180 achieved by inspecting the sample with radiography during particle delivery while remotely 181 controlling the pump. Note that the risk of tracer retention can be significantly reduced by 182 decreasing their particle size compared to the pore -throat size. While a systematic study of 183 the minimum pore throat-tracer size ratio needed to perform velocimetry experiments is out 184 of the scope of this study, preliminary tests did show significant clogging in samples where 185 the mean pore-throat size was close to the mean tracer particle diameter. As a reasonable 186 working hypothesis, we assumed that the maximum tracer size (here: 60 m, see Section 187 IIB2) should be smaller than typical pore-throat size of the main flow paths, which we 188 estimated by the mean pore-throat size in Table I. Successfully resolving smaller particles 189 could be achieved by increasing the spatial resolution of the images without impacting the 190 image quality or the temporal resolution (e.g. using synchrotron CT). 191

192 2. Particle-liquid system

The flow tracing particles were hollow glass microspheres with a nominal particle size range between 5 and 22 m and a 250 nm thick silver coating, resulting in a particle mass density of 1.4 g/ml (Cospheric, USA). We measured the particle size distribution of the tracer with a laser diffraction particle sizer (Malvern MasterSizer 3000, UK), indicating a



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Experiment	Sand pack	Porous glass
Sample		
Mean pore size (m)	172	163
Mean throat size (m)	95	78
Image-based porosity (%)	34.1	27.5
Tracer suspension		
Glycerol concentration (wt%) in water	95	93
Viscosity (cP)	523	367
Liquid mass density (g/ml)	1.247	1.242
Seeding concentration (mg/g)	8	12
Flow properties		
Flow rate (nl/min)	33	44
Interstitial velocity (nm/s)	128	212
Interstitial velocity (voxel/ time frame)	0.38	0.62
Gravitational settling for mean tracer size (nm/s)	59	85
Imaging settings		
Number of (interleaved) time frames	80	60
CT voxel size (m)	11.8	
CT image size (voxels)	658 x 658 x 539	
Acquisition time 3D images (s)	70	
Frame interval 3D images (s)	35	

TABLE I: Key experimental properties for the velocimetry experiments. Mean pore and throat sizes were based on the open-source pore network extraction algorithm PNExtract (Raeini, Bijeljic, and Blunt, 2017). Glycerol-water properties were based on tabulated data (Segur and Oberstar, 1951; Takamura, Fischer, and Morrow, 2012)

mean size of 19.3 m and the occurrence of larger sizes than the nominal range, up to 60 m 197 (Figure 2). For the velocimetry experiments, the tracer particles were suspended in high-198 viscosity mixtures of glycerol and water, with 93 - 95 weight percent glycerol. The silver 199 coating had a high X-ray attenuation coefficient due to its high atomic number, providing 200



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²⁰¹ a beneficial contrast with the liquid in the images, contrary to what can be expected from
 ²⁰² traditional micro-velocimetry particles such as polyethylene microspheres.

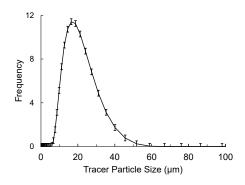


FIG. 2: We measured the size distribution of the silver coated hollow glass spheres that were used as tracer particles in the experiments with laser diffraction. The error bars reflect the standard deviation on 5 measurements.

The high-viscosity liquids caused a strong drag force on the particles, preventing that their inertia would cause deviations from the liquid's flow lines (Stokes numbers were of the order of 10^{-10} or smaller). Furthermore, the viscosity reduced the speed of gravitational settling. The terminal sinking velocity for a sphere with radius R can be calculated using Stokes' law:

$$v = \frac{2}{9} \frac{\rho_s - \rho_f}{\mu} g R^2 \tag{1}$$

with ρ_s and ρ_f the mass densities of respectively the particle and the fluid, μ the viscosity, 208 and g the gravitational acceleration (the values of these material properties are listed in Table 209 I). In the experiments, the estimated interstitial velocity (based on the imposed volumetric 210 flow rate) was two to three times higher than the settling velocity for the mean particle 211 size (Table I). In the respective experiments, particles larger than 28.5 m and 27.5 m were 212 expected to have gravitational velocities equal to or larger than the flow velocity. Note that 213 the largest of these particles may never reach the sample through the vertical tubing below 214 the flow cell. Nevertheless, gravitational settling may thus still lead to an underestimation 215 in the vertical component (along the Z-axis) of the velocity field. However, this issue can be 216 reduced by using smaller or lighter particles, or faster interstitial velocities, as the imaging 217 methods become more powerful. 218

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The particles were added to the liquid with seeding concentration of 8 or 12 mg/g (esti-219 mated 5.5 or 8.3 million particles per ml of liquid, which translates to 0.009 or 0.014 particles 220 er voxel). This was based on trial-and-error, and may be further adapted: increasing the 221 seeding concentration may lead to lower measurement times, while decreasing it may re-222 duce clogging due to jamming effects in cases where this causes issues. The suspension was 223 first vigorously stirred, then treated with an ultrasonic homogenizer (Hielscher UP50H, Ger-224 many) for 5 minutes and placed in an ultrasonic bath (Bandelin Sonorex TK52, Germany) 225 for 10 minutes to disperse the particles and remove air bubbles, respectively. The particle 226 dispersion was slightly less succesful in the sand pack experiment, likely due to technical 227 issues with the ultrasonic equipment. 228

229 C. Image processing and velocimetry analysis

230 1. Particle tracking algorithm

To track trajectories of individual particles in the time series of 3D CT frames acquired 231 during the experiment, particles were first detected in each time step image, and these 232 detections were then associated between time steps to result in particle tracks. A multitude 233 of methods to do this are compared in Chenouard et al. (2014). In this work, we used 234 the Crocker and Grier method implemented in the open-source Python package TrackPy 235 Crocker and Grier, 1996; Wel et al., 2022). First, the background was subtracted from the 236 time series images by registering and downsampling the high-quality pre-scans to the time 237 series in Avizo (Thermo Fisher, France). Then, potential particle locations were identified as 238 local grey value maxima in the background-subtracted images using TrackPy. Any particle 239 detection outside of the pore space was removed by masking the experimental images with a 240 segmentation of the pore space from the registered pre-scan (made using simple grey value 241 thresholding in Avizo). The locations of local grey-value maxima were adopted as particle 242 locations if no voxels within a minimum particle separation distance of 4 voxels had a higher 243 rey value than that maximum, and if they lied within the brightest 2 percent of grey values 244 in the pore space. These values were set by visual inspection of the particle identifications in 245 the images. The particle locations were then refined to a sub-voxel accuracy by calculating 246 the brightness-weighted centroid of the voxels in a neighbourhood around the peak value. 247



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the amount of potential matches. The association step would therefore become more chal-256 lenging if the average displacement between time frames were to be larger or if the particle 257 seeding density were to be increased. It should be noted that more advanced methods than 258 the nearest-neighbour approach have been developed, relying on e.g. multiple hypothesis 259 tracking or Kalman filtering (Jaqaman et al., 2008; Chenouard et al., 2014; Godinez and 260 Rohr, 2015). These methods are computationally more demanding, but may be of benefit 261 experiments with larger particle displacements or seeding densities than the ones pre-262 sented here. The current analysis took less than 1 hour to treat a full experimental data 263 set, running on the CPU of a moderately-sized work station (Intel Core i7-8700 with 64 GB 264 RAM). 265

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²⁶⁶ 2. Velocity field interpolation and comparison to computational fluid ²⁶⁷ dynamics

Finally, noisy particle detections with very low brightness-weighted mass were removed.

A location-prediction based nearest-neighbour algorithm was used to identify which par-

ticle observation in a certain frame most likely corresponded to a certain observation in the

previous frame (Crocker and Grier, 1996). For each particle, the local velocity was estimated

from 3 prior time steps to predict its new location in each time step (the displacement was

initialized to a user-defined value in the first time step). The observation nearest to this

predicted location was then taken as the particle's new location. To keep the calculations

tractable, a maximum search range of 6 voxels around the predicted location was set to limit

After identifying particle trajectories, those that were only a few time steps long were 268 removed, as these typically contained noisy detections. In both experiments, a minimum 269 trajectory span of 20 frames was set. Particle velocity vectors were calculated for each 270 remaining particle track using a centered finite difference approach. The resulting cloud 271 velocity vectors was then linearly interpolated on a grid with the same voxel size as 272 the experimental time step images (using SciPy), to find the 3D field of all three velocity 273 omponents. To take into account that velocities should be zero in the solid material during 274 the interpolation, zero-velocity points were added in a randomly selected fraction of the 275 ore wall voxels (2.5%). Higher-order interpolation and adding zero-points in all boundary 276 voxels was computationally prohibitive as the interpolation code remained to be optimized 277

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278 for computational efficiency.

To evaluate the measured velocity fields, we performed a cross-validation to a compu-279 tational fluid dynamics (CFD) approach to calculate the velocity fields in the pore space 280 geometry. We used an open-source finite volume solver based on OpenFOAM, from Raeini 281 and Blunt (2022). The solver performed finite-volume calculations on a hexahedral mesh 282 extracted from the segmented pre-scan of the pore space, with constant-pressure and zero-283 velocity-gradient boundary conditions at the in- and outlet. We used the standard code 284 provided by Raeini and Blunt (2022). Note that the CFD result should not be considered 285 as ground truth in this comparison, and differences compared to the experiments may result 286 from both measurement errors and numerical errors (Saxena et al., 2017). 287

288 D. Simulated CT data sets for method validation

To validate the imaging and particle tracking workflow, we generated simulated CT 289 datasets based on ground-truth particle locations. This was done by computer-generating 290 spatial distributions of analytical spheres with specified diameters and velocities, and then 291 simulating radiographs by tracing rays from a point source to a detector array through these 292 digital samples, with the tracer particle locations being updated in each radiograph. This 293 way, simulated scans contained realistic geometrical deformation and motion artifacts, as 294 particle locations changed in each radiograph (note that particle motion within individual 295 radiographs was negligible as these are typically acquired on the ms time scale). 296

The validation data was meant to mimic a velocimetry experiment in a porous medium 297 as closely as possible. To this end, we took the segmented pore geometry of the Porous 298 Glass experiment (Section IIB1) as input, and determined its CFD-based velocity field 299 see Section IIC2). The velocity field was scaled to an average velocity magnitude of 1 300 voxel per 360 scan. Then, to reflect the particle seeding of an incompressible flow, the 301 initial positions of the simulated "tracer" spheres were chosen randomly in the the pore 302 space (staying clear of the in- and outlet boundaries), with sphere radii drawn from the 303 experimentally measured tracer particle size distribution (Figure 2). The tracer seeding 304 density was tuned to approximate the Gaussian-like distribution of inter-particle distances 305 from the experiment, and was therefore also set to zero in regions with very low velocities 306 (lower than 5% of the maximum). Next, the locations of these particles were calculated as 307



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they moved through the CFD-based velocity field for 4900 time steps of 100 ms, using a 4th 308 order Runge-Kutta integration. These were the ground-truth locations for the simulated CT 309 data set, regardless of potential numerical errors in their determination (the purpose of the 310 calculation being only to create ground-truth trajectories with a realistic complexity). This 311 way, the particle positions were calculated for each radiograph time step in 7 consecutive CT 312 scans of 360 and 700 radiographs each, matching the experimental acquisition. Each of these 313 radiographs was then calculated by raytracing using the in-house developed CTRex code 314 (Heyndrickx et al., 2020; Schryver et al., 2018). Poisson noise was added on the radiographs 315 to match the noise level in the experiment. Finally, the simulated dataset was reconstructed 316 with filtered back-projection. Contrary to the experiments, there was no frame interleaving 317 in the reconstruction of the simulated data sets, to aid the interpretation and maximize 318 the generality of the results. The simulated acquisition time and frame interval were both 319 70 s. The result is a time series of simulated CT images of tracer particles moving through a 320 porous medium with exactly known trajectories, in order to investigate the errors expected 321 in the experimental data. 322

323 III. RESULTS

324 A. Experimental results

Visual inspection of cross-sections through the imaged porous media confirmed that tracer 325 particles were visible as bright spots of a few voxels in diameter, which moved slowly and 326 smoothly through the pore space (videos in Appendix). In the sand pack, tracer particles 327 appeared slightly larger, which may be due to particle aggregates being more difficult to 328 disperse in the higher viscosity liquid used for this experiment. In regions with high flow 329 rates, motion artifacts appeared to be present in the form of slightly blurred particle shapes 330 elongated in the direction of motion, rather than as severe corkscrew-shaped artifacts and 331 streaks which would occur in the case of large movements. The observed deformation did 332 not necessarily cause issues in the particle localization, as this was based on the particles' 333 grey value centroids. This will be investigated in more detail in Section IIIB. 334

Frame-by-frame particle detection yielded 2393 ± 86 particles per frame in the sand pack experiment, and 5581 ± 136 in the porous glass. Example slices through the 3D data with



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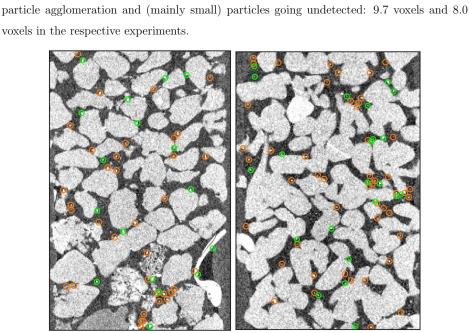
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annoted particle detections are shown in Figure 3. In the ideal scenario that there is no

particle agglomeration, the selected seeding concentrations would yield on average 1 particle

in a cube with a side length of 4.5 voxels (sand pack) or 4.1 voxels (porous glass). The

measured average distance between neighboring particles was larger than expected due to

FIG. 3: This image illustrates the frame-by-frame particle detection algorithm, applied to one 3D frame of the sandpack (left) and the glass filter (right) experiment. Detections that fall in the pictured cross-sectional slice are indicated in green, detections in a directly neighbouring slice are indicated in orange.

The identified particle locations in each time frame were linked together by the nearestneighbour algorithm, resulting in a total of 11084 (sand pack) and 50005 trajectories (porous glass), from which respectively 2490 and 4415 had the imposed minimum span of 20 time steps. 3D renderings of the filtered tracks followed tortuous paths through the pore space, as shown in Figures 4 and 5. The velocities at each point in these tracks were calculated, yielding the velocity distributions in Figure 6. The distributions of the X- and Y-velocity components perpendicular to the global flow direction were symmetrically distributed around



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³⁵⁰ zero, as expected. The mean Z-components of the measured velocities were resp. 0.54 and ³⁵¹ 0.70 voxel/frame for the two experiments (182 and 236 nm/s), compared to the interstitial ³⁵² velocities of 0.38 and 0.63 voxels/frame calculated from the injection rate (Table I). This is ³⁵³ an encouraging match, especially since the tortuosity of the pore space was not taken into ³⁵⁴ account in the interstitial velocity, meaning that the real average velocity in the pores was ³⁵⁵ likely a factor between 1 and 2 larger than the interstitial velocity (Fu, Thomas, and Li, ³⁵⁶ 2021).

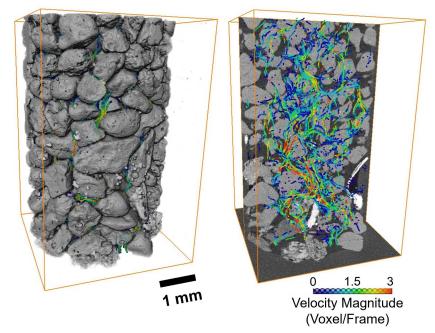


FIG. 4: Experimentally measured trajectories of tracer particles in the sand pack sample (3D rendered on the left), colored according to the velocity magnitude measured in each point (right). Only particles which could be tracked for at least 20 time frames are included.

Finally, the particle velocities were interpolated to find the velocity fields on a voxel grid. In Figure 7, we compare this to CFD simulations of the velocity field using the OpenFOAMbased solver (Raeini and Blunt, 2022) mentioned in Section II C 2. The experimental measurements and the CFD-simulations of the pore-scale velocity distributions matched well

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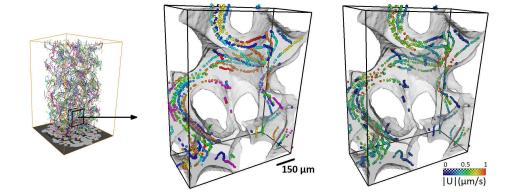
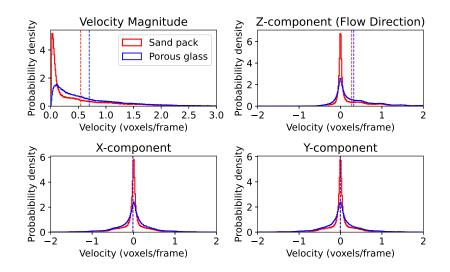
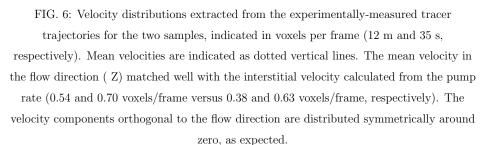


FIG. 5: A detailed view of the experimentally measured tracer trajectories in the porous glass filter sample, assigned a random color per individual particle (left and center) and colored according to the velocity magnitude |U| measured in each point (right). Only trajectories that spanned at least 20 time frames are shown.

(Figure 7). In the sand pack, mismatches close to the sample boundary may be due to inlet 361 effects: the experimental field-of-view was selected further away from the inlet than in the 362 porous glass filter, so that the exact inlet conditions could not be taken into account in the 363 simulation. In the experiments, the mean distance between all measured velocity points was 364 approximately 10 voxels, which gives an indication of the sampling density of the interpo-365 lated field. Note however that particle tracking velocimetry does not uniformly sample the 366 velocity field, as fewer observations are made in low-velocity regions. The sampling can be 367 refined by acquiring more time frames. 368









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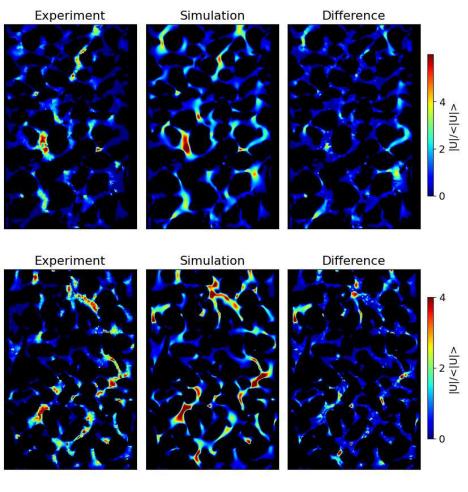


FIG. 7: Vertical cross-sections through the 3D, normalized velocity magnitude fields from the sand pack (top) and the porous glass experiment (bottom) matched well with computational fluid dynamics predictions. The figures on the right shows the absolute difference between the experimental and simulated velocity fields. Mismatches close to the sample boundary in the sand pack dataset may be due to inlet effects.

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³⁶⁹ B. Validation simulation results

Contrary to established micro-velocimetry approaches, our method used cone-beam CT data, which may suffer from specific artifacts that could impact the detection and localization of tracer particles: the geometrical deformations at the top and bottom of the volume ("cone beam artifacts"), limited spatial resolution for fast image acquisition, and motion artifacts (Cnudde and Boone, 2013; Mäkiharju *et al.*, 2022). Since the impact of these artifacts was unclear and difficult to quantify in the experimental data, we created and analyzed a digital twin of the porous glass experiment.

Figure 8 illustrates the detection of particles in the validation data set in function of 377 their size. A particle was considered to be detected if there was a detection closer than $\sqrt{3}$ 378 voxels (a voxel diagonal) from the true position. The settings used for particle detection 379 were the same as those used in the experiments, with exception of the intensity threshold, 380 which was slightly modified from 98 to 98.5% to account for the fact that the experiments 381 contained a small amount of bright particle agglomerations, which was not the case in the 382 simulations. In total, the method detected approximately 48% of the ground-truth particles 383 in individual time frames, mainly dependent on the particle size (Figure 8). Particles that 384 went undetected did not necessarily cause errors in the velocity field, but did reduce the 385 efficiency in terms of measurement time. Approximately 6 % of the particle detections could 386 not be matched to a ground-truth particle. These false detections led to errors in the velocity 387 field if they were subsequently wrongly linked into particle trajectories. Figure 8 shows the 388 ocalization error: the distance between the correct location of a ground-truth particle (at 389 time point in the middle of the acquisition) and the recovered location. Approximately 390 0% of the detected particles could be localized with an error below one voxel length (90%391 onfidence error bound: 1.02 voxels). The localization error had a median of 0.36 voxels and 392 increased significantly for smaller particles. We present these errors in units of voxels/frame 393 because we may expect similar values in experiments with other voxel sizes or frame rates, as 394 long the particle velocities scale accordingly (and the signal-to-noise ratio remains similar). 395

After linking the detected particles into trajectories and removing those shorter than 6 time steps, 33% of the true trajectories were retrieved, meaning one particle was detected within $\sqrt{3}$ voxels of the same true trajectory for at least 6 time steps. Only 9.3% of the detected tracks did not match a true trajectory. However, most of these "false positives"



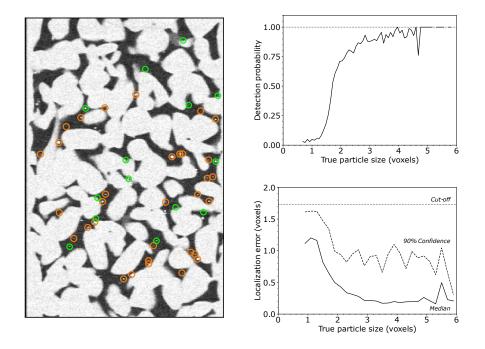


FIG. 8: On the left, a cross-sectional slice from the simulated validation data set, showing particle detections in the same slice in green and in the neighbouring slices in orange. On

the right, the detection probability (top) and the localization error (bottom) of the ground-truth particles during frame-by-frame particle identification. In total, 48% of the ground-truth particles were recovered, with a median localization error of 0.36 voxels (4.25 m) from the true particle location.

were made up of two correct parts of true tracks that were wrongly linked together, meaning they still produced at least 3 accurate velocity points for 2 incorrect ones. Less than 1% of the detected trajectories could not be matched to 1 or 2 true trajectories. Note that a more stringent length cut-off was applied in the experiments as there were more time steps available than in the simulations, which may have resulted in more accurate linking.

Figure 9 shows that the recovered and ground-truth velocity distributions in the validation data had an excellent match. By design, these distributions were also similar to the experimental velocity magnitudes in Figure 6, suggesting that similar motion artifacts and



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trajectory linking errors can be expected. In the validation data, the median absolute error 408 on the velocity magnitude was 0.072 voxels/frame, with a 90% confidence error bound of 409 0.24 voxels/frame. This was smaller than the localization error before linking suggested, 410 likely due to the rejection of low-quality detections during the length filtering, and poten-411 tially because some systematic errors in the localization may cancel out in the velocities. 412 As shown in Figure 10, the absolute error remained approximately constant for true veloc-413 ity magnitudes below 3 voxels/frame, after which the error started to increase. There was 414 no systematic over- or underestimation, but the measurement did show significant scatter: 415 the relative error bounds on the velocity magnitude (90% confidence) were approximately 416 $\pm 40\%$. The directional error, i.e. the angle between the detected and the true velocity 417 vectors, had a median value of 8.6 and a 90% confidence bound of 30.0. As shown in figure 418 10, the error angle was large where the velocity magnitude was below 0.5 voxels/frame, as it 419 was difficult to accurately quantify small particle movements because of the finite resolution 420 of the images. This was also shown by the fact that the relative error on the magnitude was 421 larger here. However, this could be improved relatively easily, for example by skipping time 422 steps in a particle's trajectory until it has moved more than a minimum set distance before 423 calculating its velocity. 425

Finally, we show the interpolated velocity field for the validation data in Figure 11, for the part of the image in which particles were seeded. Visually, the match to the simulated equivalent is comparable to that in the experiments from Figure 7, indicating the suitability of the error analyses above.





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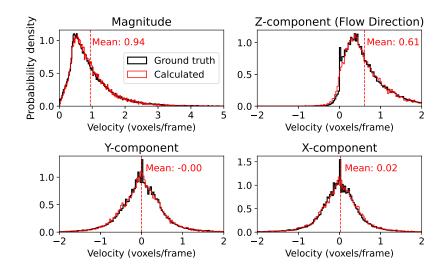


FIG. 9: Measured and ground-truth distributions of particle velocities in the simulated validation data set showed a close match.

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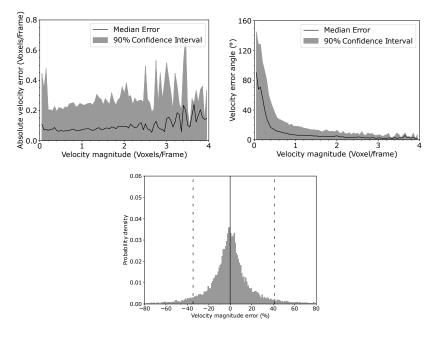


FIG. 10: Top left: point-by-point absolute velocity magnitude errors remained relatively constant below true magnitudes of 3 voxels per frame, after which they increased. Top right: there was a larger angle between the true and measured velocities for small particle displacements, i.e. at low velocity magnitudes (top right), due to the finite resolution of the images. Bottom: the histogram of the relative error on the velocity magnitude, with the 90% bounds indicated as dashed vertical lines.



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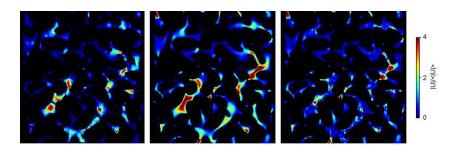


FIG. 11: In the simulated validation data set, the recovered (left) and the simulated (middle) velocity fields showed a comparable match as in the experiments. The figure on the right shows the absolute difference between the experimental and simulated velocity fields.

430 IV. CONCLUSIONS

In this paper, we present the first successful use of X-ray imaging to perform 3D ve-431 locimetry on flow in porous media. We presented two experiments on creeping, single-phase 432 flow in a sandpack and in a porous sintered glass filter, in which the paths of thousands 433 of individual tracer particles travelling through the pore space were successfully tracked. 434 The resulting velocity field matched well with a computational fluid dynamics simulation 435 on the same samples. The tracer particles used here were silver-coated spheres with a mean particle size around 20 m, suspended in a viscous liquid to slow down gravitational settling. 437 The experiments relied on continuous CT acquisition with a voxel size of 11.8 m and an 438 acquisition time of $70 \, \text{s} / 360 \, \text{scan}$, which, through an interleaved reconstruction scheme, re-439 sulted in a series of 3D images with a time (frame) interval of 35 s. The particle trajectories 440 were identified using a relatively straightforward nearest-neighbour algorithm based on an 441 open-source library (TrackPy). 442

The results were validated with the help of a digital twin of the porous glass experiment. 443 created by numerically simulating the CT imaging of particles as they move through the 444 ores. Due to the small particle size compared to the voxel size, approximately 50% of 445 the simulated particles could be detected in each image. However, particles that were large 446 enough to be detected could be localized with an accuracy below the voxel size in 90% of the 447 cases. From the recovered particle trajectories, we were able to measure velocity magnitudes 448 p to approximately 4 voxels/frame (0.69 m/s) with an error below 0.24 voxels/frame (0.04 449 m/s; 90% confidence). The recovered velocity vectors were inaccurate for small velocities 450 < 0.5 voxels/frame) as the particle displacements per individual time frame were then too 451 small compared to the resolution - an issue which may be resolved by better post-processing. 452 These validation results are expected to hold general validity towards these and other similar 453 xperiments. The main source of errors that could not be taken into account in the validation 454 were mechanical and electronic inaccuracies of the scanner. These were deemed secondary 455 to photon counting noise and motion artifacts for the fast imaging with relatively large voxel 456 sizes presented here, but may still have caused the errors in the experimental data to be 457 larger than in the validation. 458

⁴⁵⁹ Our work proves the feasibility of CT-based particle velocimetry in complex geometries, ⁴⁶⁰ and suggests that there is a large potential for further development and application of this

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method. While our measurements were limited to low flow rates, highly viscous liquids 461 and samples with large pores, these were not hard limitations. At synchrotron beam lines, 462 imaging at voxel sizes up to approximately 4 times smaller with acquisition times 100 times 463 faster have become routinely possible (Spurin et al., 2021), meaning velocities of up to 464 2orders of magnitude larger than in this work could be measured. In both laboratory-465 based and synchrotron CT, the imaging can be sped up further by advanced reconstruction 466 ethods using e.g. prior knowledge on the process (Myers et al., 2011; Eyndhoven et al., 467 2015) and motion-compensation (Schryver et al., 2018). Furthermore, the higher spatial 468 esolutions that can be achieved using these approaches would facilitate the use of smaller 469 and lighter tracer particles, thereby also easing the limitations on the viscosity of the liquid 470 and on the sample's pore size. The particle detection and linking scheme applied in this 471 paper can also still be improved using more sophisticated methods (Chenouard et al., 2014). 472 There is ample opportunity to apply all of the above concepts to CT-based velocimetry. The 473 resulting methods could bring forth a turning point in the study of fluid dynamics in complex, 474 microscopic geometries; ranging from porous materials to (bio-)medical applications and 475 industrial fluid flows. 476

477 APPENDIX

To show how tracer particles moved smoothly through the pores during the velocimetry experiments, a video of the central vertical cross-sectional slice (parallel to the flow direction) in each time frame of the porous glass experiment is provided in Figure 12 (multimedia view). The identification of trajectories on this dataset led to the videos shown in Figure 13a (multimedia view) and 13b (multimedia view), showing a detail from the full dataset, where trajectories were colored by particle or by local velocity magnitude.

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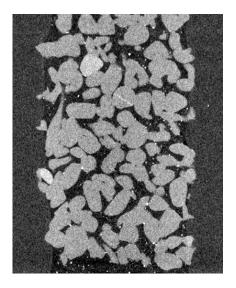


FIG. 12: A cross-sectional view of the reconstructed time frames in the porous glass experiment, showing brightly colored tracer particles (multimedia view).

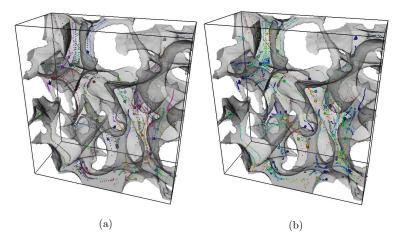


FIG. 13: Particles moving along their tracks in a detail of the porous glass dataset. In figure a (multimedia view), each individual particle is assigned a random color. In figure b (multimedia view), the color scale reflects the velocity magnitude in each point.

484 ACKNOWLEDGMENTS

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492 DATA AVAILABILITY STATEMENT

The data that support the findings of this study are freely available from Zenodo. This includes the full experimental data sets containing the 3D time frames and the resulting particle trajectory data and velocity fields:

- Sand pack experiment: http://doi.org/10.5281/zenodo.6010425
 - Porous glass experiment: http://doi.org/10.5281/zenodo.6010490
 - Validation simulations: http://doi.org/10.5281/zenodo.6010914

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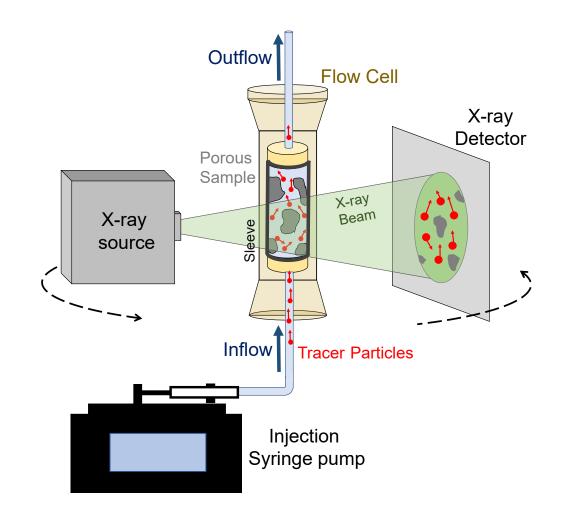


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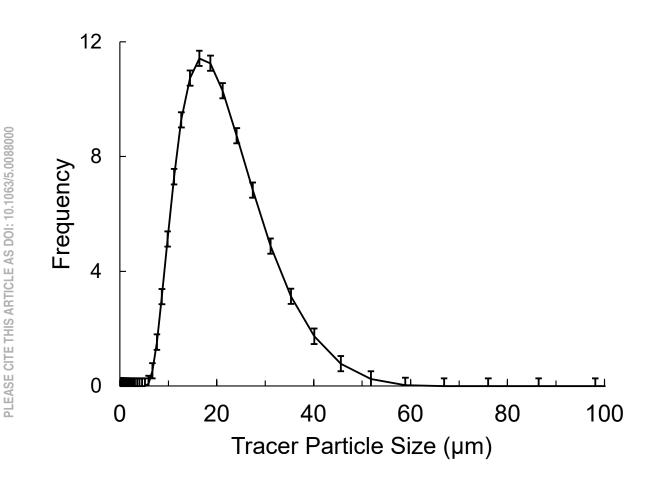
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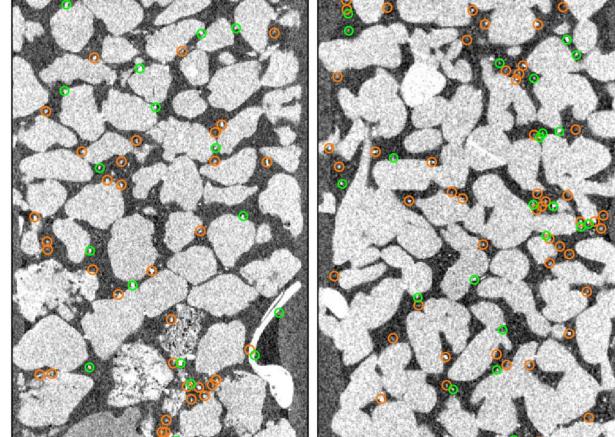




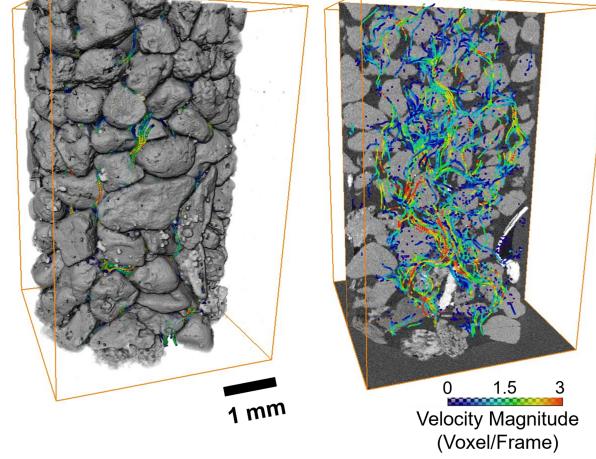


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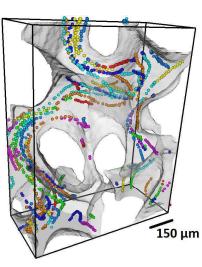
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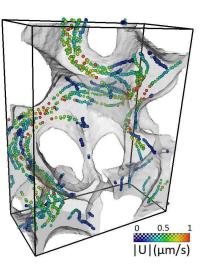




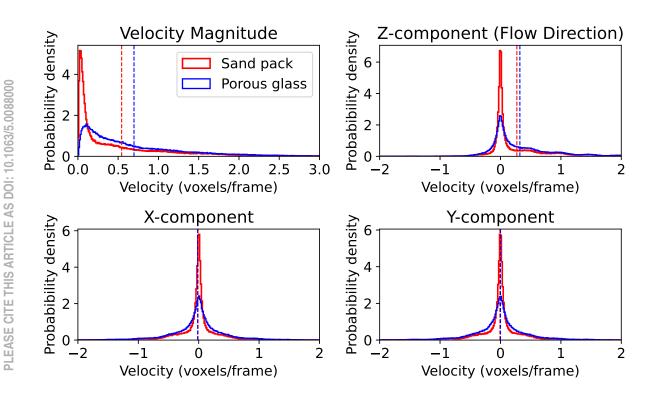








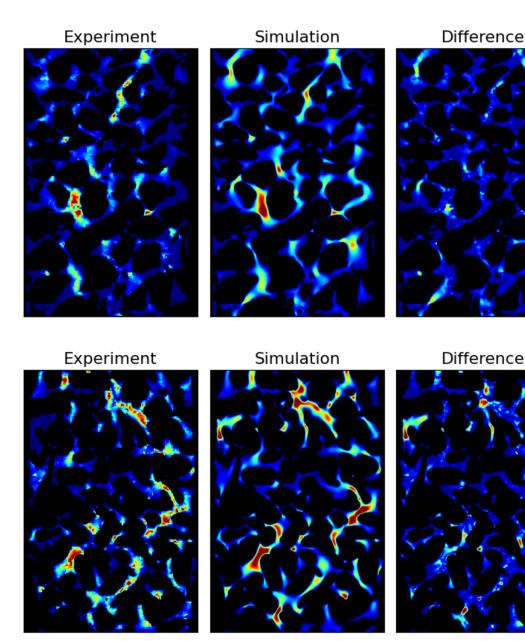






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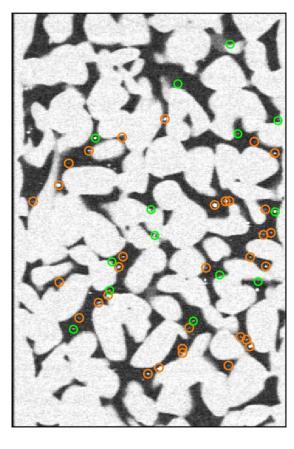


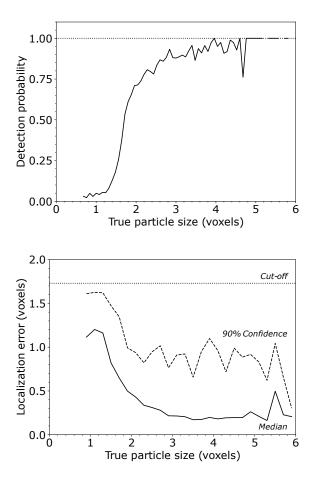
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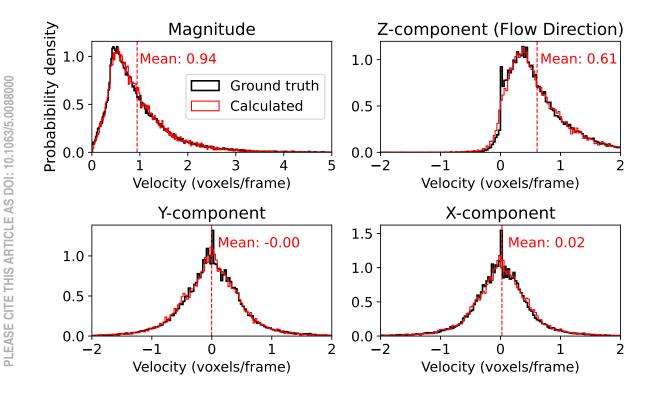


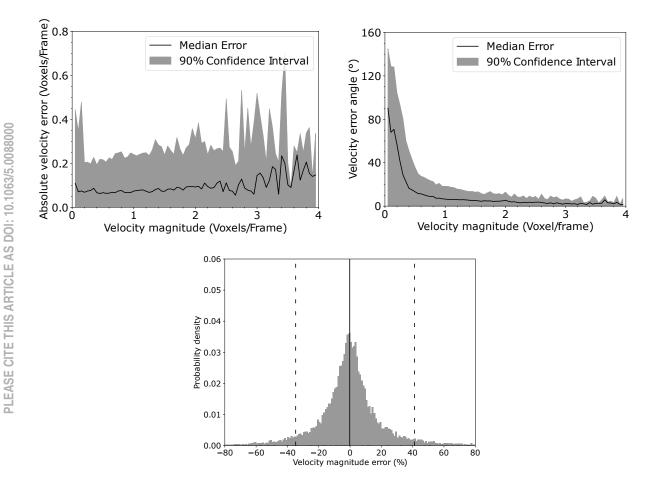
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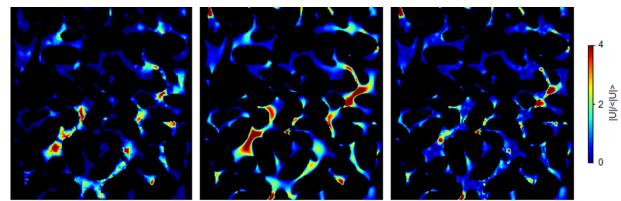






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